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The diagram illustrates a digital signal processing system for a receiver, featuring two parallel input channels and a central processing block labeled 'COMB'.

Input Channels:

- Channel 1 (Top):** Receives RF1 (Antenna Port 1) and RICPR (Reference Input for Channel 1). It includes an RF amplifier (RFAMP1), a mixer (MIX1), and a local oscillator (OL1) driven by OSCLOC. The output is IF1.
- Channel 2 (Bottom):** Receives RF2 (Antenna Port 2) and RICDIV (Reference Input for Channel 2). It includes an RF amplifier (RFAMP2), a mixer (MIX2), and a local oscillator (OL2). The output is IF2.

Central Processing Block (COMB):

- IF Stages:** IF1 and IF2 are combined in a summer (SOM) to produce IF'. IF' passes through an IF/AGC (Intermediate Frequency/Automatic Gain Control) block to produce IF. IF2 is also used to generate SF (Subcarrier Frequency) and ISF (Intermediate Subcarrier Frequency).
- Demodulation and Filtering:** IF is demodulated by a demodulator (DEM) to produce SD (Sample Data). It is also processed by a filter (F) to produce VP (Variable Phase). VP is then processed by a filter (Fn) to produce VD (Variable Delay).
- AD Converters:** Four AD converters (AD1, AD2, AD3, AD4) are used to convert analog signals to digital. AD1 and AD2 are connected to VP and VD, respectively. AD3 and AD4 are connected to the outputs of two comparators (RIV1, RIV2) which compare the signals with reference voltages (Vx, Vy).
- Digital Processing:** The digital signals from the AD converters are processed by a digital filter (ELAB) to produce RG1 (Reference Gain 1) and RG2 (Reference Gain 2). These are then processed by a digital filter (PRES) to produce TP (Time Period) and DA2 (Digital Amplitude 2).
- Output:** The final output is SD (Sample Data), which is also used to generate a reference signal (RICDIV) for the second channel.

A mixed combination strategy combiner for receivers operating in high capacity digital radio links and protected with space or angle diversity is described. The combiner comprises a system which calculates the amplitude dispersion in the spectrum of frequencies of the combined signal and a device which measures the power thereof. On the basis of this information and an appropriate calculation strategy tending to minimise the BER of the equipment, a microprocessor generates signals for gain control of the stage RF of the receivers and for phase shift control for a phase shifter for the local oscillator signal sent to one of the receivers. The calculation strategy consists of minimising a polynomial function of the power and dispersion values. Dependence of the BER on the f_{notch} characterising the dispersion is eliminated, normalising dispersion in relation to f_{notch} .

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IF Signal Combiner for Minimizing the BER in a Space or Angle Diversity Digital Radio Receiver

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DESCRIPTION

The present invention relates to radio receivers operating in digital radio links and protected with diversity techniques and more precisely concerns a mixed-combination-strategy combiner for receivers operating in high capacity digital radio links and protected with space or angle diversity.

10 As known, in a radio link connection the beam transmitted can divide into several beams which reach the receiving antenna over different paths for reasons tied to propagation. This can bring fading of the reception signal caused by the interference of the different beams on the receiving antenna. The fadings are frequently a cause of interruption of radio link connections. It is also known that the fading can be flat or dispersive. In the former case all the frequencies of the spectrum in the band of the received signal are equally attenuated. In the latter case the attenuation strikes predominantly only some zones of the spectrum, producing a distortion of the amplitude-frequency response. In reality the two types of fading can occur simultaneously.

15 It is useful to note that the dispersive fading is evaluated by measurements of dispersion in the band of the reception signal, where by dispersion it is meant the ratio between the maximum and minimum amplitudes of the frequency spectrum in said band. The frequency for which occurs the greatest attenuation is called notch frequency (f_{notch}).

20 In an individual receiver affected by fading, whether flat or dispersive, the error rate on the bits received, corresponding to the BER measured at the output of the demodulator, can exceed a certain threshold, so that the receiver is temporarily out of service. Therefore, in order to avoid this serious shortcoming, diversity reception techniques have been known for a long time. In cases of space or angle diversity, which more strictly concern the type of diversity to which the combiner which is the object of the present invention relates, reception equipment has been equipped with two or

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more receivers connected to a respective antenna or to their own feeders of said antenna. The outgoing signals from the receivers reach the inputs of a combiner which combines them appropriately to generate a single reception signal to be sent to the demodulator.

5 With the diversity criterion, the performance of the receiving equipment is considerably improved because the combined signal thus obtained has a much lower probability of going off-service than the individual signals received.

10 To implement the most appropriate combination strategy, it is essential to know theoretically and/or experimentally the transfer function of a transmitting channel affected by fading. For this purpose there have been proposed different mathematical models among which a well known model is the one proposed by Bell laboratories and known as the 'three-beam model'. Of the three beams, one is the main
15 one which reaches the receiving antenna directly, while the other two are echoes of the main beam, i.e. beams which reach the receiving antenna by completing multiple paths of different length. The transfer function proposed for the transmission channel comprises parameters whose values are inferable from knowledge of the fading
20 statistics for the particular section considered. Knowing the type of modulation of the transmitted signal, the fading statistics and the total transfer function of the entire transmission system, it is possible to obtain useful information on the signal characteristics at the output of the demodulator, e.g. power, amplitude dispersion,
25 S/N, BER, etc.

This being stated, it is the job of the combiners to act on some parameters of the diversity receivers in order to optimise a preselected characteristic of the combined signal.

30 Depending on the optimised characteristic, it is possible, generally speaking, to group the combiners in appropriate operating categories.

35 A first category includes the combiners which compensate for flat fading by carrying out a phasing of the signals present on the two antennas and then adding them together in voltage to obtain the resulting signal. This strategy corresponds to the maximum summing of the resulting amplitude. It should be clarified that by phase is intended an average phase of the received signal, coinciding with the

phase of an unmodulated spectral component transmitted in centreband by virtue of the symmetry of the modulation and the equal probability of all the states owing to the randomness of the modulating signal.

The combiners of this category are mainly used in small capacity radio links where, because of the modest band width, conditionings owing to the signal level prevail. It is natural that for large capacity radio links whose performance is more conditioned by the distortion of the amplitude-frequency response, combiners belonging to a second category characterised by tending to compensate for the dispersive fading are more useful.

These combiners perform an adjustment both of the level and the phase for the received signals, so as to obtain amplitude equality and phase opposition of the echoes on the two antennas. Subsequently the adjusted signals are added together to obtain a resulting signal in which the echoes are cancelled. Cancellation of the echoes leads to a flat amplitude-frequency response typically detectable with a spectrum analyser. However, in particular propagation situations, e.g. when the ratios between the main signal level and the level of the echoes have similar values on both antennas, the combiners of the second category are not efficient. Indeed, in the attempt to cancel the echoes, they also cancel a considerable part of the main signal, worsening the signal-to-noise ratio of the combined signal and causing a possible increase in the down time of the equipment.

To overcome the limitations of the previous combiners, combiners belonging to a third and a fourth category have been developed which set out to optimise the overall performance of the system while allowing for flat and dispersive fading.

Combiners of the third category are characterised by the fact that, based on the fading characteristics of the received signals, they switch from one type of operation, tending to compensate for the flat fading, to the type tending to compensate for the dispersive fading. This manner of operating however brings an excessively fast passage between the two operating zones which, as has been amply shown, can cause oscillations not tolerated by the demodulator.

Combiners belonging to the fourth category, which adopt a mixed combination strategy, also try to obviate this shortcoming in the attempt to compensate simultaneously for the flat and dispersive

fading.

An example of a diversity reception system adopting said mixed combination strategy is described in Italian patent application no. 22531A/88 for Telettra, inventors Rocco Nobili, Francesco Rasà and
5 Dario Sormani, filed 7 November 1988.

Said known application claims a system for combining at least two received signals under diversity conditions involving at least two receivers, a combiner for signals coming from said receivers and a demodulator, characterised in that there is used a combiner
10 arranged upstream of the demodulator which measures the power and dispersion of the signal combined therein and destined for the demodulator. On said signal it also makes a calculation of BER with intermediate frequency and, on the basis of the BER value thus calculated, acts in an adaptive and dynamic manner on the two signals
15 received depending on the minimization of said BER.

The system is also characterised in that the BER is calculated with the following function based on experimentally obtained results:

$$BER = 10^{\alpha P + \beta} + 10^{\gamma D + \delta}$$

where P and D are the measured values of the power and dispersion of
20 the combined signal and the parameters α , β , γ , δ are characteristics of the modulation system employed.

The combiner used in the Telettra system is not however without shortcomings, and in particular it does not seem that it eliminates in a definitive manner the shortcoming resulting from generation of
25 oscillations in the combined signal. The cause of this could be the excessive steepness of the exponential functions used to represent the two contributions to the BER, together with the fact of having neglected the 'mixed' term, i.e. dependant simultaneously on power and dispersion. Indeed, as better explained below, the function
30 claimed tends to maintain the combiner in the combination state for maximum power even in the presence of a fair dispersion contribution, then passing suddenly into the combination state for the slightest dispersion when the dispersion contribution becomes excessive. This applies evidently also for the contrary behaviour. In practice, it
35 is as though the combiner in question switched from one type of operation to the other, as happens for the third category combiners.

It can thus be inferred that the mixed combination strategy

seems to be hardly effectively implemented by the Telettra combiner and the greatest gaps occur unfortunately just in the intermediate zone of the power and dispersion values where said strategy should bring the greatest benefits.

5 A second possible shortcoming is due to the fact that, in the presence of notch frequencies suddenly variable because of peculiar dispersive fading situations, the system could have trouble converging toward the minimum BER values, or not converge at all. Indeed, in the $BER(P,D)$ function, there is not shown the further
10 dependence thereof on the notch frequency values, to which refer the dispersion values D given on the abscissa of the chart in FIG. 5 of the above mentioned patent. The nature of said dependence is better explained below. The assertions concerning the second shortcoming are supported by the fact that, while in the Telettra application
15 there is expressly stated that the algorithm used for minimization of the BER minimises the function $BER(P,D)$ given above, nothing is said about the type of algorithm used. There are thus no elements for affirming that said algorithm can effectively minimise also a function representing the BER in a more realistic manner, i.e. which
20 also considers its dependence on f_{notch} .

Accordingly the purpose of the present invention is to overcome the above shortcomings and indicate a mixed combination strategy combiner for receivers operating in high capacity digital radio links and protected with space or angle diversity.

25 To achieve said purpose the present invention has for its object a signal combiner for radio receivers operating in digital radio links and protected with space or angle diversity. The combiner in question acts downstream of the intermediate frequency stages of the radio receivers and upstream of the demodulator. It comprises a
30 system which calculates the dispersion of the amplitude in the frequency spectrum of the combined signal and a circuit which measures the power in the spectrum of said signal. On the basis of this information and of an appropriate calculation strategy tending to minimise the BER at the demodulator output, a processing unit
35 processes phase shift values, for a phase shifter which phase shifts with each other the local oscillator signals used by the receivers for conversion to intermediate frequency of the respective radio

frequency signals, and commands to change the gain of the RF stage of the receivers. The calculation strategy consists of minimising an appropriate objective function of polynomial type, in which the independent variables are the values of power and amplitude dispersion of the signal at the output of the combiner. The dependence of the BER on f_{notch} which characterises the dispersion is almost completely eliminated by performing a normalisation of the dispersion values which enter into the objective function, as better described in the first claim.

5 The combiner of the present invention has the great advantage of making the reception equipment in which it is used considerably insensitive to the fadings of the reception signal caused by the multiple paths of the transmitted signal. The effectiveness of its operation is also especially appreciable when the two types of fading occur simultaneously and when the dispersion is characterised by notches rapidly changing within the spectrum.

10 Other purposes and advantages of the present invention are clarified by the detailed description given below of an example of embodiment thereof and the annexed drawings given by way of nonlimiting example in which:

FIG. 1 shows a block diagram of reception equipment in space diversity in which the block COMB represents the signal combiner which is the object of the present invention;

FIG. 2 shows the BER curves of reception equipment provided in accordance with the known art and a BER curve of the equipment of FIG. 1;

FIG. 3 shows other BER curves similar to those of FIG. 2;

FIGS. 4 to 7 show the flow chart of a program controlling the operation of the combiner COMB of FIG. 1.

30 With reference to FIG. 1, APR and ADIV indicate two receiving antennas belonging to space diversity radio reception equipment comprising also two receivers RICPR and RICDIV connected to the antennas APR and ADIV respectively, an oscillator OSCLOC, a signal combiner COMB and a demodulator DEM.

35 The signal reaching the two receiving antennas is a microwave signal consisting of a carrier modulated by a 155Mbit signal in accordance with a 128 TCM modulation format. However the combiner

COMB is capable of operating equally well with other QAM modulation formats.

The antenna APR receives a signal RF1 which reaches a variable gain radio frequency amplifier RFAMP1 constituting the input stage of the receiver RICPR. Analogously the antenna ADIV receives a signal RF2 which reaches a second variable gain radio frequency amplifier RFAMP2 constituting the input stage of the receiver RICDIV.

The outputs of the amplifiers RFAMP1 and RFAMP2 are connected to first inputs of two frequency converters MIX1 and MIX2 respectively, to whose second inputs arrive a local oscillator signal OL1 generated by OSCLOC and a signal OL2 derived from OL1 respectively by appropriate phase shifting. At the outputs of the converters MIX1 and MIX2 are present two respective signals IF1 and IF2 corresponding to the conversion of the signals RF1 and RF2 to an intermediate 70MHz frequency.

The intermediate frequency signals IF1 and IF2 reach two distinct sum inputs of an adder SOM at whose output is present a sum signal IF' which reaches the input of an intermediate frequency amplifier IF/AGC having automatic gain control. At a first output of IF/AGC is present an amplified intermediate frequency signal IF which reaches a demodulator DEM having at its output a demodulated signal SD.

On either one of the two ways which join the outputs of the converters MIX1 and MIX2 with the respective inputs of the adder SOM is inserted a delay line, not visible in FIG. 1, consisting of a section of coaxial cable of appropriate length which equalises the absolute delay existing between the intermediate frequency signals IF1 and IF2 because of the different length of the paths which they cover to reach the inputs of the adder SOM.

The adder SOM and the amplifier IF/AGC are part of a block COMB which constitutes the signal combiner which is the object of the present invention. The combiner COMB also includes a processor ELAB, a dispersion measurement system MISDISP, a phase shifter circuit SF for the signal of the local oscillator OL1, an interface ISF toward said phase shifter circuit SF, four analog/digital converters AD1, AD2, AD3 and AD4, two digital/analog converters DA1 and DA2, and finally two detector circuits RIV1 and RIV2.

The amplifier IF/AGC has a second output for a signal VP which represents the appropriately amplified voltage which controls amplification of IF/AGC. Said voltage is approximately inversely proportional to the power of the signal IF' and thus represents a measurement of the power of said signal.

The network MISDISP measures the amplitude dispersion in the spectrum of the signal IF and also supplies an indication of the position of the frequency for which amplitude attenuation of IF is maximum (f_{notch}). Said measurements are available separately at two outputs of the system MISDISP. More precisely at a first output is present an analog signal VD which represents the dispersion value and at a second output is present a signal Fn which represents the value of f_{notch} .

The signals VP and VD output from IF/AGC and MISDISP reach the analog/digital converters, respectively AD1 and AD2 whose digital signals in output reach a first and a second input gate of the processor ELAB. The signal Fn reaches directly a third input gate of ELAB.

The intermediate frequency signals IF1 and IF2 reach the detectors RIV1 and RIV2 whose outputs are connected to the analog/digital converters AD3 and AD4. The digital signals issuing from AD3 and AD4 reach a respective fourth and fifth input gate of ELAB.

The processor ELAB generates at a first and a second output gate two signals RG1, RG2 which control the gain of the input stages RFAMP1 and RFAMP2 of the receivers RICPR and RICDIV. For this purpose the signals RG1 and RG2 reach the digital/analog converters DA1 and DA2 whose outputs are connected to respective gain control inputs of the radio frequency amplifiers RFAMP1 and RFAMP2. The latter control their gain in a known manner.

The phase shifter SF has a first input to which arrives the local oscillator signal OL1 which is phase shifted by SF and sent to the output as signal OL2. The direction of the phase shift of the signal OL1 is controlled by a digital signal PRES which issues from a third output gate of the processor ELAB and reaches a first input of the interface ISF. The magnitude of the phase shift of OL1 is determined by a timing Tp, also generated by ELAB and sent to a

second input of ISF. The interface ISF has two outputs from which issue two isofrequential sinusoidal in-quadrature signals Vx and Vy which reach respectively a second and third input of the phase shifter SF.

5 The interface ISF includes an address generator for an EPROM in which are memorized samples of the signals Vx and Vy, two latch-registers in which are memorized the data read in the EPROM, two digital/analog converters connected to the outputs of said registers, two filtering and amplification circuits connected to the
10 outputs of the digital/analog converters and a circuit which synchronizes the reading of the EPROM and conversion to analog operations.

 There is now explained the operation of the combiner COMB inserted in the diversity reception equipment of which it is a part.
15 In operation, as known, the two receiving antennas APR and ADIV are separated by a distance such that the fadings on the respective beams received are poorly correlated. The reception signals RF1 and RF2, whose characteristics are described above, are sent to the input stages RFAMP1 and RFAMP2 of the respective receivers RICPR and RICDIV
20 of which RICPR is the main one and RICDIV the diversity one. The receivers RICPR and RICDIV are positioned downstream of their respective antennas and are connected to the feeders by a waveguide and appropriate branching filters. Because of their particular positioning, RICPR and RICDIV are also called 'front end'.

25 The radio frequency signal issuing from RFAMP1 is converted into the signal IF1, at the intermediate frequency of 70MHz, by the frequency converter MIX1 which it uses for conversion of the local oscillator signal OL1. Similarly, the radio frequency signal issuing from RFAMP2 is converted into the signal IF2 at the intermediate
30 frequency of 70MHz by the frequency converter MIX2 which it uses for conversion of the local oscillator signal OL2. The phase shifter SF shifts the signal OL2 appropriately in relation to OL1, and this is translated into a relative phase shift between the two intermediate frequencies IF2 and IF1.

35 The variable gain radio frequency amplifiers RFAMP1 and RFAMP2, just as the local oscillator OSLOC and the frequency converters MIX1 and MIX2 are of known type. The phase shifter SF is also of known

type and is embodied by an image rejection mixer.

The signals IF1 and IF2 are added together to obtain the combined signal IF', whose power level is amplified and stabilised by the intermediate frequency amplifier IF/AGC which is also of known type. The combined signal IF issuing from IF/AGC is demodulated by the demodulator DEM to obtain the starting digital signal. In view of this, it is useful to note that the combination operation does not consist of merely summing IF1 with IF2, because a basic role is played by the strategy according to which the levels of the signals IF1 and IF2 are controlled. The adjustments must be such that they eliminate or minimise any type of fading in the combined signal IF. For the combiner in question the control strategy consists principally of the acquisition by the processor ELAB of the signals VP1, VP2, VP, VD and Fn and an appropriate processing thereof in order to generate in output the control signals RG1, RG2, Tp and PRES.

The above control strategy relates to the mixed combination "philosophy" and, as explained for FIGS. 2 and 3, consists essentially of minimising an appropriate objective function of the independent variables VP, VD and Fn. The behaviour of the objective function approximates that of a family of curves representing constant BER values, measured at the output of the demodulator DEM, having VP, VD and Fn as parameters. The block ELAB of the example is provided in a nonlimiting manner by the INTEL microprocessor 80C31.

The signals VP1, VP2, VP, VD and Fn which reach ELAB come from measurements made on the intermediate frequency signals IF1, IF2, IF' and IF. More precisely, the signals VP1 and VP2 indicate the power of the individual signals IF1 and IF2 and hence, keeping into account the known amplifications or attenuations introduced by RFAMP1 and RFAMP2, that of the reception signals RF1, RF2. Said powers are obtained by detection and filtering operations of IF1 and IF2 completed by the respective blocks RIV1 and RIV2, which include detection circuits of known type. The signal VP represents the power of the combined signal IF' measured immediately after the output of the adder SOM. The measurement of VP is made in a known manner by the automatic gain control circuit (AGC) included in the amplifier IF/AGC and in practice the voltage of AGC is used. It should be

noted that, because of the mixed combining strategy implemented by the combiner COMB, the voltage VP might not represent the sum of the powers of the signals IF1 and IF2. Indeed, the sum signal IF' is affected by the phase shift between IF1 and IF2 introduced by the phase shifter SF.

The signals VD and Fn issuing from the measurement system MISDISP represent the amplitude dispersion in the spectrum of the signal IF and the notch frequency which characterises said dispersion respectively. The processor ELAB calculates the relative position of f_{notch} in the IF spectrum performing the relationship $F_n' = F_n / f_{\text{symbol}}$, because f_{symbol} coincides with the known value of the band width B of the signal IF. For example, if f_{notch} falls in the centre of band B, then $F_n' = 0$. But if f_{notch} falls at the ends of the band, then $F_n' = 0.5$ because the band ends are characterised by the values of $\pm f_{\text{symbol}}/2$.

The circuitry embodiment of the system MISDISP is already known to those skilled in the art and its description is therefore not considered necessary. It is however useful to note an innovative example of an embodiment of said system recently implemented in the laboratories of the applicant. For this embodiment, there was filed in the name of Siemens Telecomunicazioni, an Italian patent application No. MI92A 002341, dated 12 October 1992, entitled 'Device for calculating the amplitude dispersion of the spectrum of a modulated signal' in which are designated the same inventors as for the present invention.

As concerns the control signals RG1, RG2, Tp and PRES generated by the processor ELAB, it should be first noted that the characteristics of the signals Tp and PRES depend on how the phase shifter SF acts to phase shift the signal OL1, while for the digital signals RG1 and RG2 there is nothing to add to that which had already been stated.

A phase shifter which uses an image rejection mixer must necessarily have an input for the local oscillator signal OL1, to be phase shifted, and two inputs for two isofrequentional sinusoidal signals mutually phase shifted 90° , as are the signals Vx and Vy. That stated, representing by f_1 the frequency of OL1, f_m the frequency of Vx and Vy, and f_2 the frequency of the output signal

OL2, will be $f_2 - f_1 \pm f_m$, where the sign + or - depends on the fact that V_x and V_y are mutually phase shifted $+90^\circ$ or -90° . The difference $|f_m|$ between the frequencies f_1 and f_2 produces an absolute phase shift value between the input and output of the phase shifter which increases constantly in time. Indeed, the phase shift expression is $|2\pi f_m t|$. Of course if $f_2 > f_1$, the signal OL2 anticipates OL1 and vice versa in the contrary case. The phase shifting process continues until the value established by the processor to compensate for the fading is reached, after which it is stopped and the phase shift remains at the value reached. Phase shifting is stopped merely by stopping the generation of V_x and V_y .

In view of the foregoing, the interface ISF must generate the two sinusoids V_x and V_y only during predetermined time intervals and must also be able to interchange the signals V_x and V_y on the two outputs to reverse the direction of the phase shift. For the first purpose it makes use of the signal T_p , while for the second purpose it makes use of the signal PRES. When the signal T_p is high, generation of V_x and V_y is enabled but when it is low at the outputs of V_x and V_y , there is present a constant value corresponding to that of the respective values existing upon disabling. The signal PRES is a bit written by ELAB in a special output register.

The address generator belonging to the interface ISF consists of a two way counter timed by an oscillator signal coming from the internal timing circuit. At each increase of the counter there is performed a first reading of the EPROM and the first word read is memorized in a first latch. Immediately afterward but before the new increase of the counter, the logical value of the last address bit of the EPROM is negated in order to perform a second reading in another memory zone of a second word which is memorized in a second latch. The sequence of the first words read constitutes the temporal succession of samples of the sinusoid V_x , while the sequence of the second words constitutes that of V_y .

The signal T_p reaches the counting enablement input of said two way counter, enabling or disabling reading of the EPROM and hence generation of V_x and V_y . The signal PRES reaches the input pin of the counter which determines the direction of counting forward or backward. It can be easily shown that by reversing the direction of

reading of the EPROM the sinusoids V_x and V_y are interchanged on the outputs and the direction of the phase shift is also reversed.

The phase shifter SF of the example is capable of producing a phase rotation of the signal OLI with a rate of 6000 degrees per second, obtained with a frequency f_m of the sinusoids V_x and V_y of approximately 16.6Hz. The combiner COMB is able to follow flat fadings characterised by attenuation speeds which can reach even 1000 dB/sec and dispersive fadings characterised by notches which move through the band of IF at a speed which can reach 300MHz/sec. The only limitation to the speed of the combiner is due to the time constant of the AGC included in the amplifier IF/AGC.

With reference to FIG. 2 there is noted a chart in which on the abscissa are shown the flat fading values FF and on the ordinates those of dispersive fading DA. The values of FF and DA are expressed in dB and are calculated by ELAB by means of the expressions: $DA = -20\log VD$; $FF = 20\log(VP_{max}/VP)$ where VP_{max} is the maximum value taken by the voltage VP during an appropriate period of observation under nominal propagation conditions.

The chart shows a family of curves FAM1 and two curves identified by S and T not belonging to FAM1. The family FAM1 represents the function $\log BER(FF, DA) = \text{constant}$. The BER is that measurable at the output of the demodulator of a generic digital receiver, not necessarily in diversity, to which arrives a modulated signal QAM transmitted on a path affected by flat and dispersive fading. For each curve of the family is indicated the value of the constant, i.e. of the parameter $\log BER$, for which the curve was plotted. The family FAM1 can also be interpreted as a group of level curves of a surface represented by the function $\log BER(FF, DA)$ traced in three-dimensional Cartesian space. In this case the distance between the level curves gives an indication of the steepness of the function.

Two lines: $FF = FF_1$ and $DA = DA_1$ divide the Cartesian plane of the variables FF and DA in four zones, i.e. identified by I, II, III and IV respectively for the purposes explained below.

The family FAM1 gives a very explanatory and at the same time concise indication of how the performance of a generic receiver can be influenced by the fadings which unavoidably appear on the section.

Said family is the result of a computer simulation but can be inferred by appropriate mathematical manipulation of known curves or can be obtained directly by experimentation.

The curves identified by S in said figure represents the
5 function $\log\text{BER}(\text{FF}, \text{DA}) = \text{constant}$, evaluated at the output of the demodulator of the reception system of FIG. 1. The curve S was obtained by computer simulation of a diversity system comprising the complete circuitry diagram of FIG. 1. In the simulation the signals are combined in accordance with the polynomial formula set forth
10 below. In the calculations were introduced the values of $\log\text{BER} = -4$ and $f_{\text{notch}}/f_{\text{symbol}} = 0$.

The curve indicated by T represents the function $\log\text{BER}(\text{FF}, \text{DA}) = \text{constant}$ evaluated at the output of the demodulator of the reception system described in the Telettra patent application mentioned above.
15 The curve T was obtained by computer simulation of a diversity system comprising the complete circuitry diagram proposed by Telettra in which the combiner operates in accordance with the related exponential formula. For a correct comparison with the curve S, in the calculations was used the same value of $\log\text{BER} = -4$.

20 The chart of FIG. 2 is however not complete. Indeed, in the calculations which lead to the plotting of the family FAM1 the values of the dispersive fading DA, indicated on the ordinate, are for a notch which falls in centre band ($F_n' = f_{\text{notch}}/f_{\text{symbol}} = 0$). These values can however be obtained with notches falling in different
25 positions within the band, influencing differently the BER. More complete information therefore requires introduction of F_n' into the calculation as the second parameter which allows for the relative position of the notch used to simulate the dispersion. The computer simulations in which this further dependence is taken in due
30 consideration lead to plotting of new curve families, a family for each new value of F_n' , but which for the sake of simplicity are not shown in additional figures. The new curve families are all similar in form to FAM1 but are gradually translated upward with the increase in the values of F_n' . The maximum translation is on average
35 approximately 3dB and is found for $F_n' = 0.5$, i.e. when the notch falls at the band ends. In addition, again with the increase in the values of the second parameter F_n' , the individual curves inside each

family are more widely spaced. The explanation of this behaviour is that when the notch moves to the band ends the system becomes less sensitive to dispersive fading.

From the totality of all the above considerations it can thus be concluded that the BER of a receiver to which arrives a signal affected by fading is well represented by a family of curves for each value of f_{notch} .

The utility of this representation becomes more understandable below, i.e. when the problem of determining the shape of the mathematical function which implements the better mixed-combination strategy is used and furthermore each time it is useful to take advantage of a 'visual' representation of how the combiner COMB acts in minimising the BER at the output of the demodulator DEM.

With reference to FIG. 3 there are noted three curves indicated by A, B and C respectively in the Cartesian plane of the variables FF, DA. The curve A corresponds to the curve of FIG. 2 belonging to the family FAM1 identified by the value of $\log \text{BER} = -4$ and $F_n' = 0$. The curve C corresponds to a curve, not shown in FIG. 2, having the same value of $\log \text{BER}$ for curve A but belonging to a family identified by the value $F_n' = 0.5$. Between the curve A and the curve C are included infinite curves corresponding to the values of F_n' variable with continuity from 0 to 0.5. The area between curves A and C indicated by Z_{ac} shows the dependence of the family of curves on the parameter F_n' . The curve indicated by B represents the new position of the curve C after appropriate normalisation of the values of the variable DA, performed with the purpose of reducing the dependence of C on the parameter F_n' . The area between the curves A and B indicated by Z_{ab} shows the residual dependence of curve A on the parameter F_n' after normalisation. As may be seen in the figure, normalisation of the variable DA achieves very well its purpose and indeed the area Z_{ab} is considerable less than the area Z_{ac} . Using DA^* to indicate the normalised value of DA, the formula applied for said normalisation is as follows:

$$(1) \quad DA^* = (\underline{k} \times DA^2) + (DA \times \underline{h})$$

with $\underline{k} = 0.0518 \times F_n'/2$ and $\underline{h} = -0.043 \times F_n'/2$, taken experimentally and depending on the type of modulation.

Application of the formula (1) leads back all the possible curve

families to a single family characterised by the function $\log\text{BER}(\text{FF}, \text{DA}^*) = \text{constant}$.

For the following remarks, which are preliminary to determination of the objective function, it is useful to refer to FIGS. 2 and 3. Examining the family FAM1 it can be noted that by varying the parameter $\log\text{BER}$, the individual curves pass progressively and without break from one to the other. The same applied for the dependence of the entire families of curves of the parameter Fn' . This behaviour is explained by the fact that the function $\log\text{BER}(\text{FF}, \text{DA})$ in the field where it has practical significance, is continuous and monotonically growing with the growth of the values of the variables FF , DA and the parameter Fn' . In addition, the charting of the family FAM1 shows a very similar trend between the different curves, which can be better investigated by examining the curves in the individual zones I, II, III and IV.

Zone I is characterised by low flat fading values FF and by high dispersive fading values DA and in this zone the curves have a trend almost parallel to the axis of the abscissa. Therefore the BER is dependant mainly on the dispersive fading.

Zone II is characterised by intermediate values of the variables FF and DA and in this zone the BER is strongly influenced by both fading types.

Zone III is characterised by low values of dispersive fading DA and high flat fading values FF and in this zone the curves have a slightly sloped trend compared with the axis of the ordinates but the BER depends mainly on the flat fading FF .

Zone IV is characterised by low values of both flat fading FF and dispersive fading DA and in this zone the BER remains almost constant and close to minimum values.

From the foregoing the meaning of the terms FF_1 and DA_1 is clear. More specifically, the former corresponds to a value of FF above which the flat fading must be taken into consideration. The latter corresponds to a value of DA above which dispersive fading must be taken into consideration.

The above remarks concerning the zones I, II, III and IV and the terms FF_1 and DA_1 apply naturally also in the reference to the normalised family $\log\text{BER}(\text{FF}, \text{DA}^*) = \text{constant}$, not represented in the

figures, but whose charting is similar to that of FAM1. For the above said family the reference to FIG. 2 continues to apply also.

With the intention of applying the best mixed combination strategy, the way followed was to select an objective function of the polynomial type in the variables FF and DA* capable of approximating as well as possible the average trend of the curves of FAM1. This choice brings an immediate advantage due to the fact that the polynomial function is simple and easy to manage with the calculations. A second advantage is that minimization of the BER is faster and more effective, thanks to the particular trend preselected for the polynomial function. Indeed, said trend reproduces well the reaction of the receiver to an objective physical reality, i.e. that in which the fadings are never either only of the flat type or only of the dispersive type. This stated, the objective function calculated by the processor ELAB is as follows:

- (2) $OB(FF, DA^*) = OB1(FF) + OB2(DA^*)$ where:
- (3) $OB1(FF) = (FF - a)^2$ for $FF > FF_1$ and $DA^* > DA_{1*}$;
- (4) $OB1(FF) = (FF + b)$ for $DA^* \leq DA_{1*}$;
- (5) $OB2(DA^*) = c(DA^* - d)^2$ for $DA^* > DA_{1*}$;
- (6) $OB2(DA^*) = (mDA^* + q)$ for $DA^* \leq DA_{1*}$ and $FF \geq FF_1$.

In expressions 3 and 4 the term FF_1 is that indicated in FIG. 2. In 5 and 6 the term DA_{1*} has a value approximately equal to the term DA_1 of said figure.

Functions 2 to 6 are given as a nonlimiting example of a possible objective function of polynomial form: a more refined approximation of the family FAM1 could require addition of additional terms of a higher degree. The values of the coefficients a, b, c, d, m and q , depending on the type of modulation, are calculated to obtain the best possible approximation of the curve S of FIG. 2.

The objective function 2, according to the values of the variables FF and DA*, generates a family of objective curves appropriately spaced from each other and all similar in form to the single curve S shown in FIG. 2.

The family of objective curves has no dependence on the parameter F_n' because the polynomial function is calculated using the normalised dispersion variable DA*. It follows that thanks to the similarity of FAM1 to the family of objective functions, the

objective function minimization process leads also to minimization of the function $\log \text{BER}(\text{FF}, \text{DA}^*)$ and hence of the BER at the output of the demodulator DEM.

FIG. 2 gives a visual aid useful in understanding the operation of minimization of the BER, which consists indeed of searching for the shortest path to unite two curves starting from any point on a generic curve to reach an immediately underlying curve. Examining in particular the minimization process in zone II, in which the variables representing the two types of fading take on intermediate values, it is noted that the curves of type S of the objective family have a curvature such that, during the search for the minimum, the two types of fading are both adequately considered.

Therefore this zone, which is more critical for the known combiners, is not critical at all for the combiner COMB, which always acts in accordance with an effective mixed combination strategy. The same cannot be said for the Telettra combiner, which acts on the basis of a family of curves similar to curve T, which in zone II shows a sharp change of slope.

Of course, when the minimum BER falls in zone II, it does not correspond to a situation of maximum power nor to a situation of minimum dispersion. It corresponds rather to an optimised combination of the two situations.

FIGS. 4 to 7 show the flow chart of a program implemented by the microprocessor INTEL 80C31 which constitutes the processing block ELAB. The program controls the combiner COMB and the reception equipment of FIG. 1 of which the combiner is a part. The program structure does not at all reflect that of programs which use known algorithms for seeking the minimum of a function. It is much more articulated and more in harmony with the implementation of a minimum search strategy performed by trial and combining appropriately terms whose values change in an un foreseeable manner. Said strategy consists mainly of introducing appropriate perturbations in some physical parameters of the receivers and evaluating the impact thereof on the objective function values and those of flat and dispersive attenuation measured individually and modifying adaptively the number and/or intensity of said disturbances until reaching an optimal flat or dispersive attenuation condition such that the

objective function does not diminish further.

The above remarks are further clarified by the explanation of the flow chart wherein:

- in steps 1 and 2 are carried out some operations of initialization of the RAM and some internal registers of the microprocessor, called also hereinafter unit, concerning the frequency f_{symbol} , the constants FF_1 and DA_1 which delimit the four zones, the coefficients k and h , of the expression used for normalisation and finally the coefficients a , d , m and g , of the objective function.
- In the next step 3 the unit seeks the maximum value VP_{max} of the signal VP which it then uses to calculate the variable FF ;
- in step 4 the unit reads the input data, i.e. the numerical values corresponding to the input signals VP_1 , VP_2 , VP , VD and F_n ;
- in step 5 there is carried out a test on VP and VD ; if the values read remain constant, the program goes back to the preceding step 4, otherwise it continues in step 6 wherein it calculates the values of the variables FF , DA , F_n' , DA^* and then the objective function $OB(FF, DA^*)$;
- in step 7 the unit generates appropriate values of the output signals T_p , $PRES$, RG_1 and RG_2 . The signals T_p and $PRES$ command a predetermined phase shift of the signal OL_1 . The signals RG_1 and RG_2 activate gain control of the front-end amplifiers (F-END) $RFAMP_1$ and $RFAMP_2$. Said control is done for two reasons: first, to avoid saturation of the front-end amplifiers when the level of the signals received is too high, and second, to activate the best mixed combination strategy during minimization of the objective function. For this purpose, if the dispersion VD is very low, the signals RG_1 and RG_2 are such as to avoid the saturation of $RFAMP_1$ and $RFAMP_2$. But if the dispersion VD is detected, only the gain of the amplifier which receives the most attenuated signal is increased. This allows better cancellation of the echoes which is done after acting only on the step of OL_1 . The program then performs steps 8 and 9 which are similar to steps 4 and 6. Steps 7, 8 and 9 are repeated several times during the program because they are attempts made by the unit to minimise the

BER of the equipment.

- The next step 10 is a test if the value of the objective function is constant: if it is, there is calculated in step 11 a test of the value of the dispersion VD to determine if at the same time it has increased. If VD has not increased, in step 12 the test on VD is repeated to determine if it has remained constant or has decreased. If VD has remained constant, in step 13 a test on the power VP of the combined signal is completed to determine if it has decreased: if VP has not decreased, a sequence including three steps 16, 17 and 18 initiates, starting from a point C, exactly like the three steps 7, 8 and 9. If from the tests on VD completed in steps 11 and 12 the dispersion has decreased, the program goes from step 12 directly to point (C), skipping step 13.

15 - Returning to the test of step 10, if the objective function has not remained constant, there is completed in step 14 another test of the value of said function. If the latter has decreased, the program returns to point (C), and if the objective function has increased step 15 is performed in which the unit generates a command which presets the phase shifter SF to reverse the sign of the phase shifting of the signal O11, after which the program continues at point (C). The program performs step 15 even in those cases in which, in step 11, VD has increased, and, in step 13, VP is constant or has decreased.

20 - After performance of phases 16, 17 and 18, the program completes in step 19 a test of the value of the objective function to see if it has decreased. If it has, the program goes back to point (C), but otherwise goes to step 20 where the test on the objective function is repeated to determine if it has remained constant or increased.

30 - If the tests of steps 19 and 20 show that the objective function has increased, the program returns to point (E). If the function has remained constant, there is completed in step 21 a test on the dispersion VD. If VD has increased, in step 22 a test of the power VP is performed namely if VP is greater than an upper limit, such that the flat fading FF is less than the value FF₁. In practice, it is tested if the combiner is working

in zone I or IV of FIG. 2. If it is, the program proceeds to point (E) and thence to performance of steps 23 and 24, which are exactly like steps 15 and 7, after which there is a jump to point (A) in the initial part of the program. If in step 22, VP is less than or equal to the above upper limit, it means that the combiner is working in zone II or III of FIG. 2, and there is then a jump to point (F), which precedes performance in step 25 of a test of the dispersion VD.

If the test performed in step 21 showed that the dispersion VD had not increased, the program went directly to step 25, skipping steps 22, 23 and 24. In step 25 it is asked if VD is less than a value such that DA is less than the value DA₁. In practice it is tested if the combiner is working in zone III or IV of FIG. 2. If not, it means that the combiner is working in zone I or II of FIG. 2, and in this case, in step 26, there is completed a test of the power VP to see if the combiner is working in zone I or II of FIG. 2. If it is working in zone I, the program skips to point (G), but if the combiner is in zone II, the program performs a sequence of three steps 27, 28 and 29 which are exactly like 7, 8 and 9 and whose beginning is marked by a point (H). If the test of step 25 shows that the combiner was working in zone III or IV of FIG. 2, the program went directly to performance of the sequence of steps 27, 28 and 29, skipping step 26.

At the end of step 29 the program enters step 30 in which a test of the value of the objective function is performed: if the function has decreased, there is a jump to point (C), and otherwise in the next phase 31 there is performed another test to see if the function has increased or remained constant. In the former case there is a jump to point (E), while in the second case the program performs, in step 32, a test on VP exactly like that performed in step 26.

If the test of step 32 shows that the combiner is working in zone I or IV of FIG. 2, the program goes into step 33 in which a test on VD is completed exactly like that of step 25. If the additional test of step 33 shows that the combiner is working in zone I of FIG. 2, there is a jump to point (E), and otherwise it

means that the combiner is in zone IV of FIG. 2: in this case the program goes to step 34. If the test of step 32 showed that the combiner was working in zone II or III of FIG. 2, the program went directly to step 34, skipping step 33.

- 5 - In step 34 a test on the power value VP is completed: if it has decreased, there is a jump to point (E), and otherwise there is a jump to point (H).
- If the two tests completed in steps 25 and 26 showed that the combiner was working in zone I of FIG. 2, the step 26 returned to point (G) in which the program performs the sequence of steps 35, 36 and 37, which are exactly like 7, 8 and 9, and then goes into step 38.
- 10 - Step 38 is a test of the value of the objective function: if this is decreased, there is a jump to point (C) at the beginning of the program, but otherwise the program goes to step 39 where there is completed another test to determine if the objective function has remained constant or has increased. In the former case a jump to point (E) is performed, but otherwise the program goes to step 40 in which a test on the power VP is completed, like the test completed in steps 26 and 32;
- 15 - if the test of step 40 shows that the combiner is now working in zone II or III of FIG. 2, in step 41 another test on the power VP is performed to determine if it has decreased; if step 40 shows that the combiner is working in zone I or IV of FIG. 2,
- 20 - the program goes directly from step 40 to step 42, skipping step 41; but if step 41 is performed and shows that VP has decreased, there is a jump to point (H) but otherwise step 42 is performed in this case also.
- 25 - Step 42 is a test on the dispersion VD to determine if it has increased: if it has, there is a jump to point (E). Otherwise the program goes into step 43 where there is performed another test on the dispersion VD, to determine if it has remained constant or decreased: in the former case there is a jump to point (F), while in the latter case there is a jump to point
- 30 (G).
- 35

The detailed description of the flow chart of the program together with the information available in the programming and operating

manuals of the microprocessor indicated or of an equivalent one allow a person skilled in the art, particularly expert in the use of microprocessors, the embodiment of the combiner which is the object of the present invention.

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CLAIMS

1. Signal combiner for radio receivers operating in digital radio links and protected with space or angle diversity, placed downstream of two radio receivers and upstream of a demodulator, comprising: an adder (SOM) which sums the IF signals issuing from the radio receivers, obtaining a combined signal (IF') having a residual power attenuation and a residual amplitude dispersion because of propagation conditions; a network (MISDISP) which measures the residual amplitude dispersion (DA) and the position (Fn) of the frequency f_{notch} such that the residual amplitude attenuation in the spectrum of the combined signal is maximum; a device (IF/AGC) which measures the power of said combined signal (VP) from which said residual power attenuation (FF) is calculated, characterised in that it comprises a digital signal processor (ELAB) which:

- receives the results of said measurements;
- generates control signals adaptively varied, respectively for the gain of variable gain radio frequency amplifiers, constituting the input stage of said radio receivers, and for the reciprocal phase shift of the local oscillator signals, for frequency conversion stages of said radio receivers for generation of said intermediate frequency signals;
- calculates optimised values of a polynomial function (OB(FF, DA*)) of said residual amplitude dispersion (DA) and of said residual power attenuation (FF) of the combined signal, so minimising the BER at the output of said demodulator (DEM), said optimised values being obtained through said adaptive variation of the control signals;

also characterised in that said residual amplitude dispersion (DA*) of said polynomial function corresponds to said measured residual amplitude dispersion (DA) subjected to a normalisation which reduces drastically a further dependence of said polynomial function on said frequency f_{notch} .

2. Signal combiner in accordance with claim 1, characterised in that said digital signal processor (ELAB) calculates said optimised values of said polynomial function by minimization of said polynomial function in accordance with the following expression:

$$OB(FF, DA^*) = OB1(FF) + OB2(DA^*)$$

where: $OB1(FF) = (FF - a)^2$ for $FF > FF_1$ and $DA^* > DA_1^*$

$$OB1(FF) = (FF + b) \text{ for } DA^* \leq DA_1^*$$

$$OB2(DA^*) = c(DA^* - d)^2 \text{ for } DA^* > DA_1^*$$

$$OB2(DA^*) = mDA^* + q \text{ for } DA^* \leq DA_1^* \text{ and } FF \geq FF_1$$

and wherein: FF is said residual power attenuation of the combined
 5 signal; DA^* is said normalised residual amplitude dispersion; FF_1 is
 a limit value of FF below which said BER at the output of the
 demodulator depends predominantly on DA^* ; DA_1^* is a limit value of
 DA^* below which said BER at the output of the demodulator depends
 predominantly on FF; a, b, c, d, m and q are coefficients such that a
 10 parametric representation $OB(FF, DA^*) = \text{constant}$ of said polynomial
 function approximates in the best way a parametric representation
 $\log BER(FF, DA^*) = \text{constant}$ of said BER;
 also characterised in that said digital signal processor (ELAB)
 calculates said adaptive variation of the control signals through
 15 perturbations thereof of such a value as to obtain said minimization
 of the polynomial function.

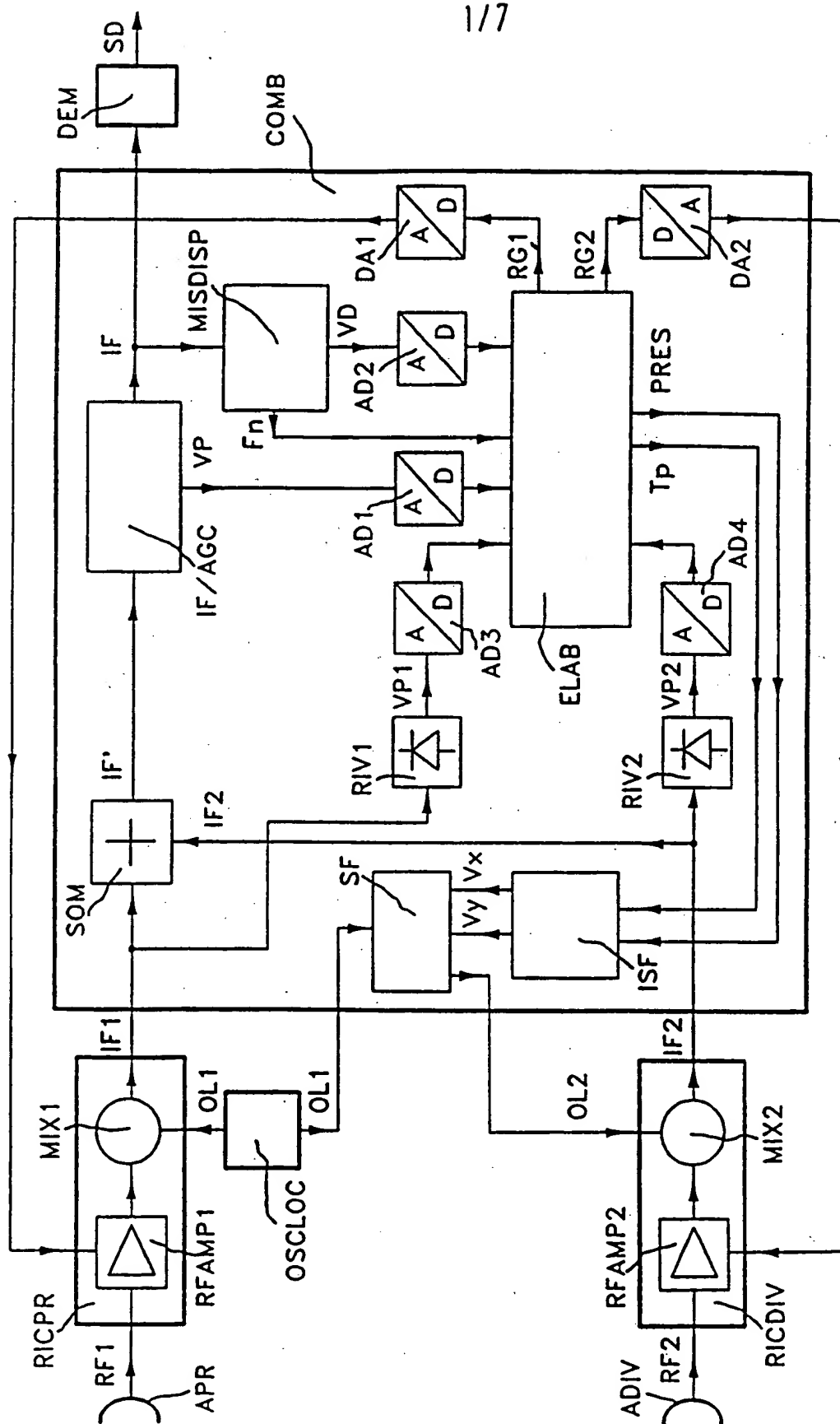
3. Signal combiner in accordance with claim 1, characterised in
 that said normalisation of the measured values of said residual
 amplitude dispersion (DA^*) has the following expression:
 20 $DA^* = (N1 \times (2f_{\text{notch}}/B) \times DA^2) + (DA \times N2 \times 2f_{\text{notch}}/B)$
 where DA and DA^* are said residual amplitude dispersions measured and
 normalised respectively, B is the band width of said combined signal
 (IF'), N1 and N2 are values taken experimentally.

4. Signal combiner in accordance with claim 1, characterised in
 25 that said combiner (COMB) also includes means (RIV1, RIV2) which
 measure the power of said intermediate frequency signals ($IF1, IF2$)
 issuing from said receivers (RICPR, RICDIV), and make them available
 to additional inputs of said processor (ELAB) for calculation of said
 adaptive values of said gain control signals (RG1, RG2) of said radio
 30 frequency amplifiers (RFAMP1, RFAMP2),
 and in that said adaptive values calculated by said processor (ELAB)
 are such that when said measured residual amplitude dispersion (DA)
 is high they cause an increase in the gain of a radio frequency
 amplifier which receives a more attenuated signal, facilitating said
 35 optimisation of said polynomial function.

5. Signal combiner in accordance with claim 1 characterised in
 that said processor (ELAB) is a microprocessor.

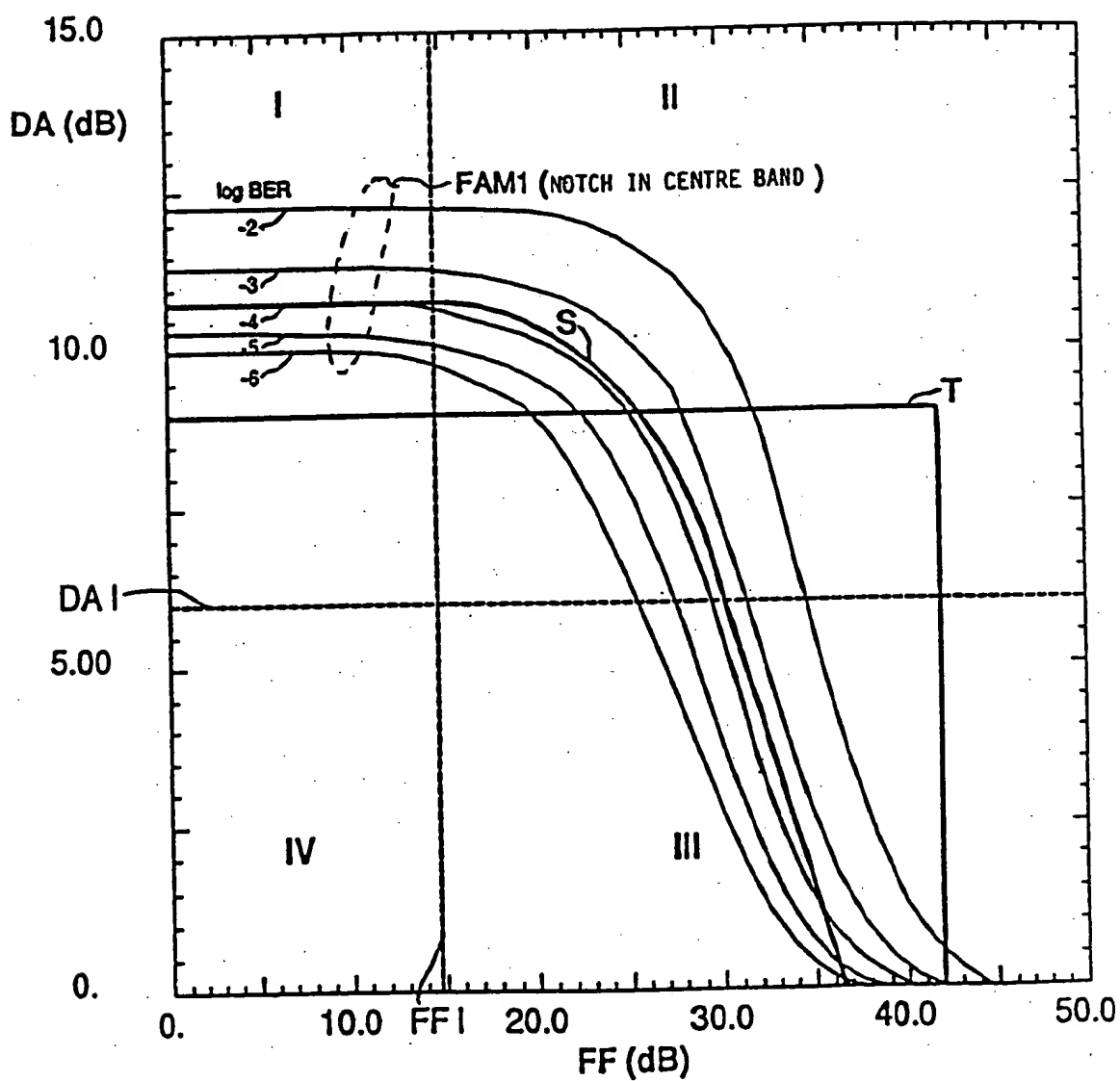
1/7

FIG 1



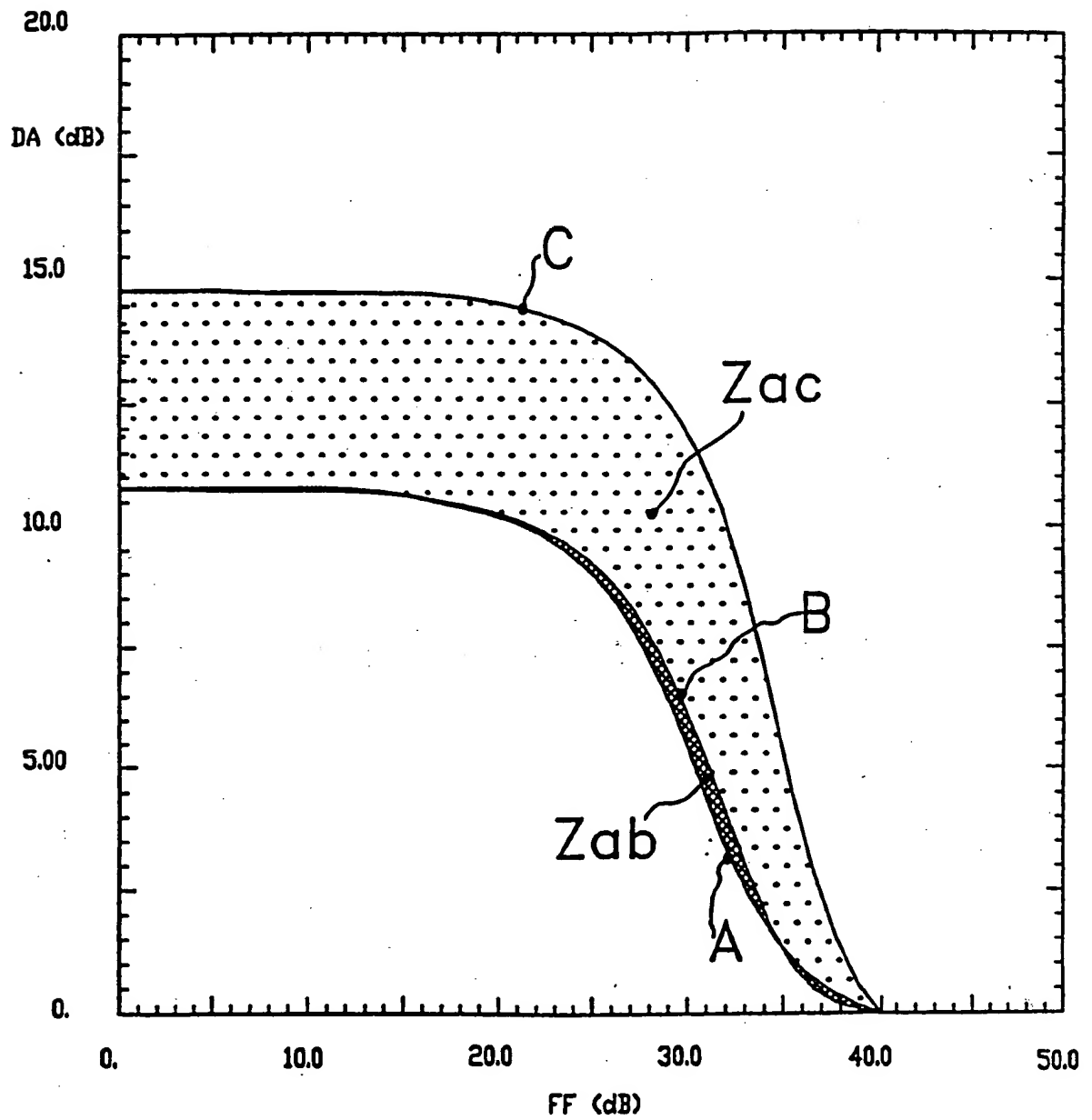
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FIG 2



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FIG 3



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FIG 4

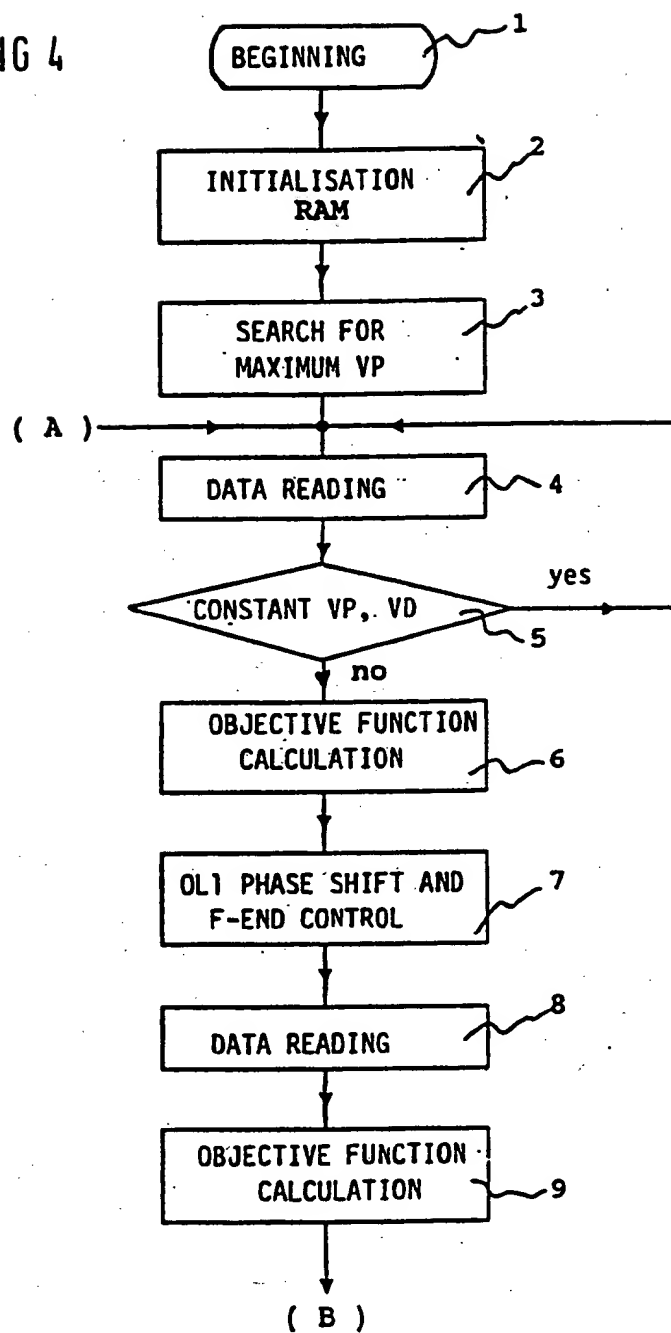
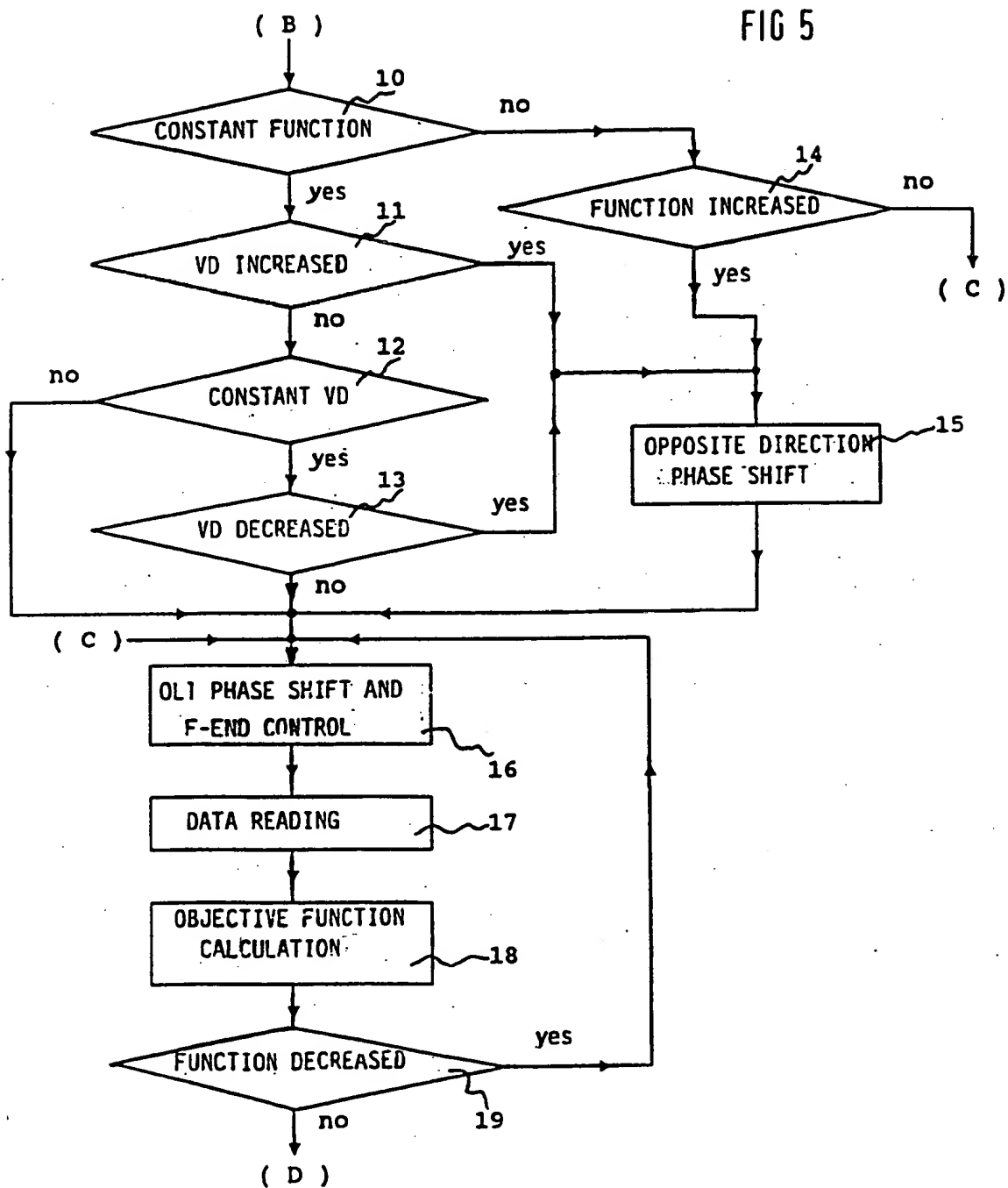
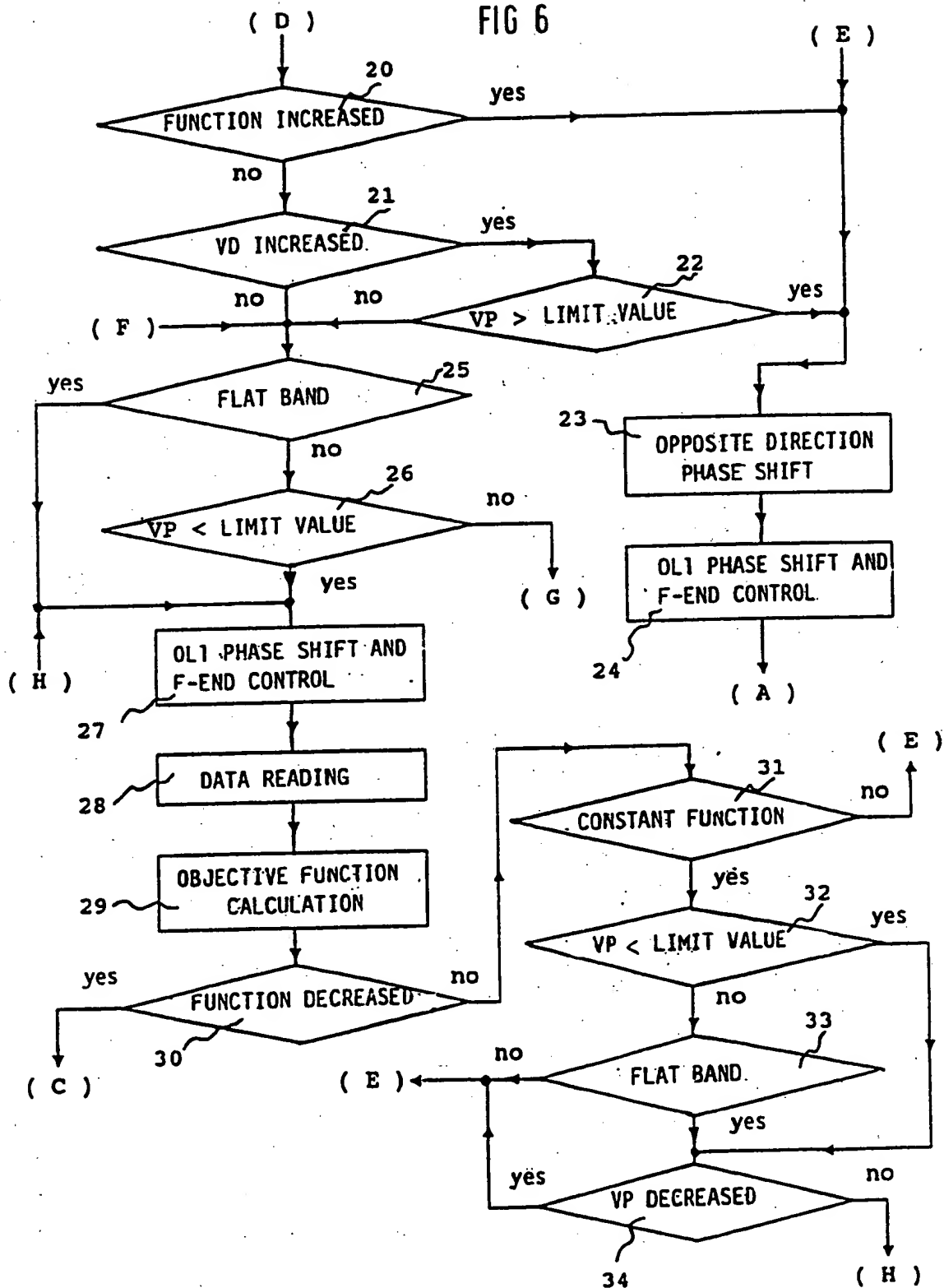


FIG 5



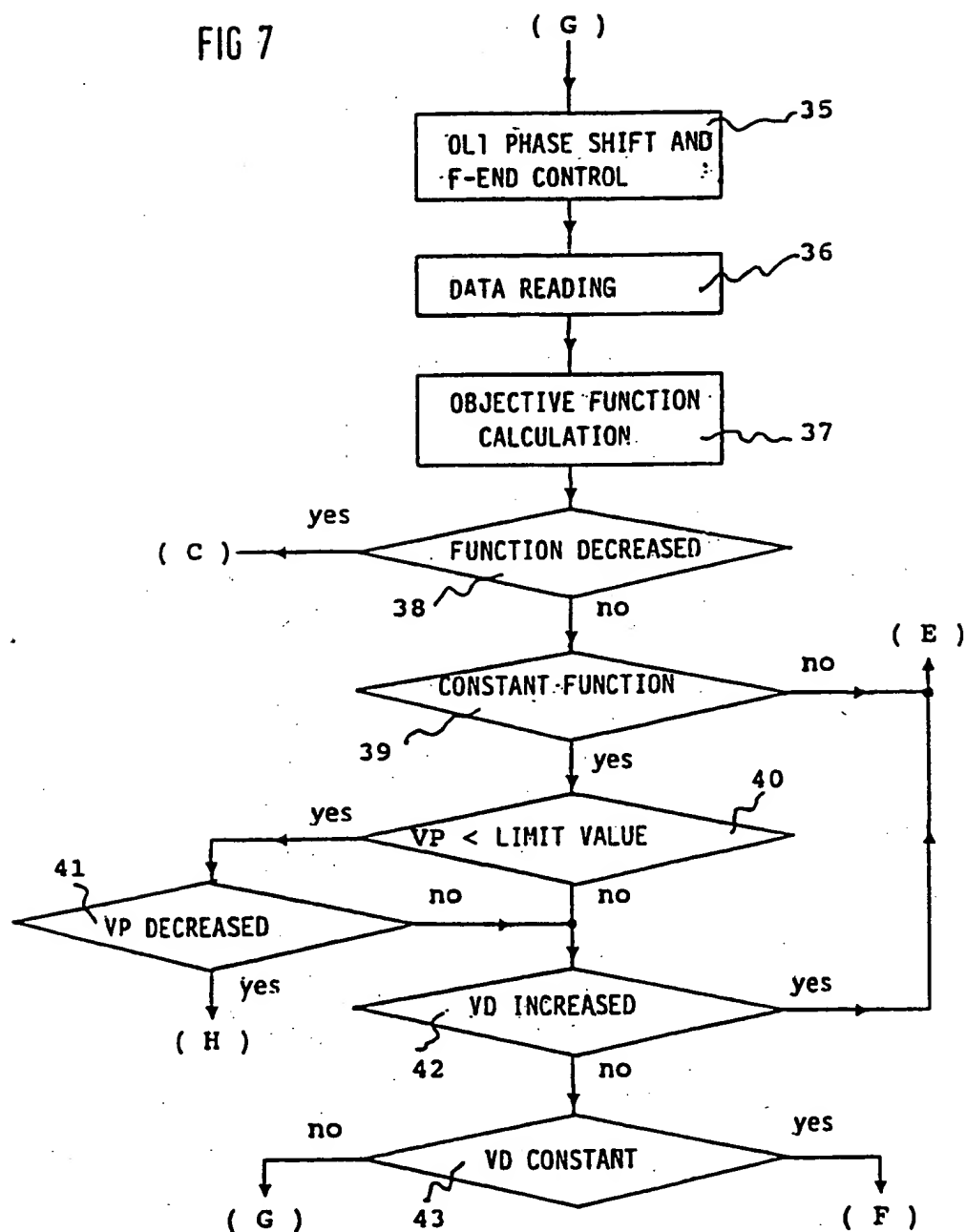
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FIG 6



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FIG 7



INTERNATIONAL SEARCH REPORT

Intern. Application No
PCT/EP 93/02758

A. CLASSIFICATION OF SUBJECT MATTER
IPC 5 H04B7/08 H04L1/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 5 H04B H04L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	PROCEEDINGS OF 22nd EUROPEAN MICROWAVE CONFERENCE 24-27 August 1992, Espoo (FIN) TUNBRIDGE WELLS (UK) volume 2, pages 1143-1148; U.CASIRAGHI ET AL.: "MIBS IF COMBINER FOR SPACE AND ANGLE DIVERSITY IN DIGITAL RADIO: FIRST TRIAL RESULTS" see abstract see page 1143, line 1 - line 42 see figure 1 ---	1,5
A	IT,A,1 227 559 (TELETTRA) 16 April 1991 cited in the application see page 4, line 14 - page 5, line 7 see page 6, line 1 - page 10, line 11 see figure 6 ---	1,5
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☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
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- "O" document referring to an oral disclosure, use, exhibition or other means
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- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
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Date of the actual completion of the international search

27 January 1994

Date of mailing of the international search report

11.02.94

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C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	PROCEEDINGS OF GLOBECOM 86 1-4 December 1986, Houston, Texas (US) NEW YORK (US) pages 1856-1860, S.NAKATANI ET AL.: "ONE HUNDRED KILOMETER OVERWATER SPAN DIGITAL RADIO SYSTEM - LS-200M SYSTEM" see page 1859, left column, line 28 - right column, line 16 see figure 6 ---	1
A	COMMUTATION ET TRANSMISSION vol. 13, no. 3, October 1991, PARIS FR pages 61 - 76 XP262699 O.DE LUCA & B.HURINVILLE "NEW GENERATION 140 AND 155Mbit/s DIGITAL MICROWAVE SYSTEM" see page 65, middle column, line 1 - line 38 see page 71, middle column, line 1 - right column, line 17 see figures 2,7 -----	1,5

PCT/EP 93/02758

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
IT-A-1227559		NONE	

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